

Program: RFEM 5, RFEM 6, RSTAB 8, RSTAB 9, RF-FE-LTB, FE-LTB

Category: Second-Order Analysis, Isotropic Linear Elasticity, Warping, Member

Verification Example: 0050 – Cantilever Under Torsion Without Warping

0050 – Cantilever Under Torsion Without Warping

Description

A thin-walled cantilever of QRO-profile is fully fixed on the left end ($x = 0$), and the warping is enabled. The cantilever is subjected to a torque M at $x = L_1$ according to the **Figure 1** [1]. The problem is described by the following set of parameters.

| | | | | | |
|----------|----------------|-----------------------|-------|------------|-----|
| Material | Steel | Modulus of Elasticity | E | 210000.000 | MPa |
| | | Shear Modulus | G | 81000.000 | MPa |
| | | Plastic Strength | f_y | 355.000 | MPa |
| Geometry | QRO Cantilever | Length | L | 4.000 | m |
| | | Width and Height | b | 200.000 | mm |
| | | Face Thickness | t | 6.000 | mm |
| Load | | Torque | M | 80.000 | kNm |
| | | Position | L_1 | 2.800 | m |

Small deformations are considered and the self-weight is neglected. Determine the maximum rotation $\varphi_{x,\max}$ and control the values of the moments $M_{T_{\text{pri}}}$, $M_{T_{\text{sec}}}$ and M_{ω} at the point $x = L_1$.

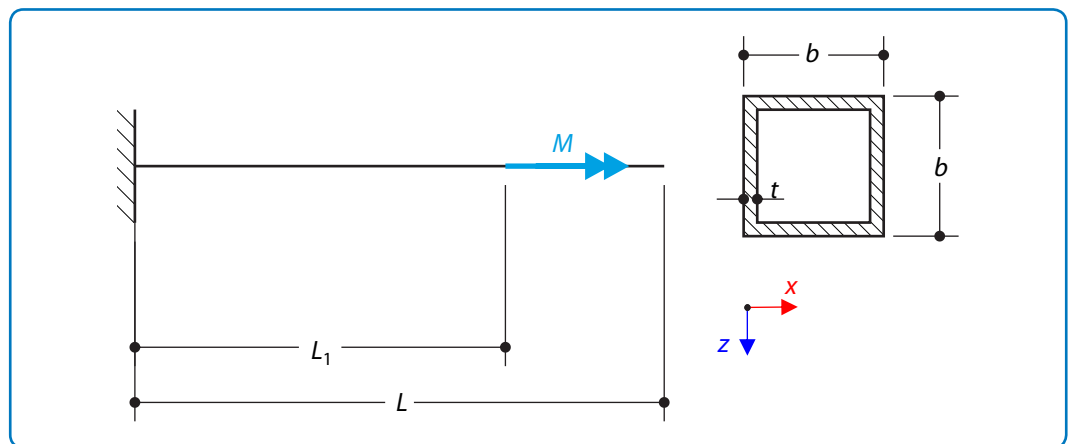


Figure 1: Problem sketch

Analytical Solution

The relative twist ϑ of the cantilever can be calculated according to the following formula

$$\vartheta = \frac{M}{GJ} = 2.252 \cdot 10^{-5} \text{ rad/mm} \quad (50 - 1)$$

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where J is the torsional constant¹. For the given profile it is

$$J = 4.386 \cdot 10^7 \text{ mm}^4 \quad (50 - 2)$$

The maximum rotation about the x axis $\varphi_{x,\max}$ occurs at the point $x = L_1$ and it has the same value to the free end.

$$\varphi_{x,\max} = \vartheta L_1 = 0.063 \text{ rad} \quad (50 - 3)$$

For this thin-walled profile (radii in the corners are neglected) is the warping constant $C_\omega = 0$. Thus the moments $M_{T\text{sec}}$ and M_ω , which are defined below, should be zero on the full length of the profile. The primary torsional moment $M_{T\text{pri}}$ should be coincident with the total torsional moment M_T .

$$M_\omega(x) = -EC_\omega \varphi'(x) \quad (50 - 4)$$

$$M_{T\text{sec}} = \frac{dM_\omega(x)}{dx} \quad (50 - 5)$$

RFEM and RSTAB Settings

- Modeled in RFEM 5.05.0029, RSTAB 8.05.0029 and RFEM 6.01, RSTAB 9.01
- The element size is $l_{FE} = 0.200 \text{ m}$
- The number of increments is 5
- Isotropic linear elastic material model is used
- The structure is modeled using members
- Second-Order Analysis is used
- RF-FE-LTB and FE-LTB module is used in RFEM 5 and RSTAB 8
- Torsional Warping and Steel Design add-on is used in RFEM 6 and RSTAB 9

Results

| Structure Files | Program | | | | |
|--------------------------|----------------------------|-------------------|-------|-----------------|-------|
| 0050.01 | RFEM 5 – RF-FE-LTB, RFEM 6 | | | | |
| 0050.02 | RSTAB 8 – FE-LTB, RSTAB 9 | | | | |
| | Analytical Solution | RFEM 5, RF-FE-LTB | Ratio | RSTAB 8, FE-LTB | Ratio |
| $\varphi_{x,\max}$ [rad] | 0.063 | 0.063 | 1.000 | 0.063 | 1.000 |

¹ The torsional constant for the given profile can be approximately calculated as $J_{\text{approx.}} = t(b - t)^3$. The exact value is taken from RFEM / RSTAB.

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| | Analytical Solution | RFEM 6 | Ratio | RSTAB 9 | Ratio |
|--------------------------|---------------------|--------|-------|---------|-------|
| $\varphi_{x,\max}$ [rad] | 0.063 | 0.063 | 1.000 | 0.063 | 1.000 |

In the following graphs there is demonstrated the behaviour of all the moments on the given cantilever calculated in RF-FE-LTB or FE-LTB module. The primary torsional moment $M_{T\text{pri}}$ should be coincident with the total torsional moment M_T . The moments $M_{T\text{sec}}$ and M_ω should be zero on the full length of the profile. It can be seen there is the affected area in the nearby of the loading point ($x = L_1$), when the warping is considered. Note that the above mentioned effect is getting smaller with the smoother mesh.

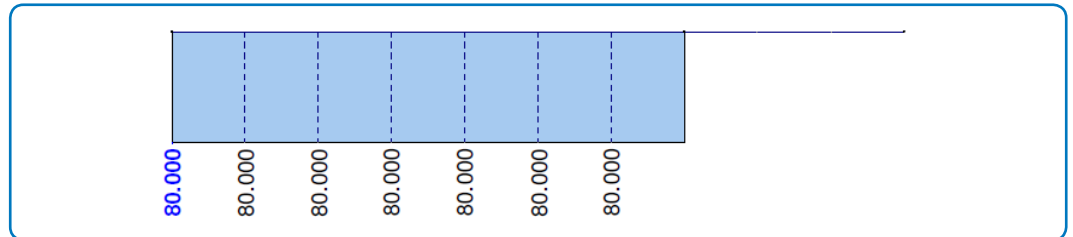


Figure 2: RFEM 5 – Total torsional moment M_T [kNm] behaviour

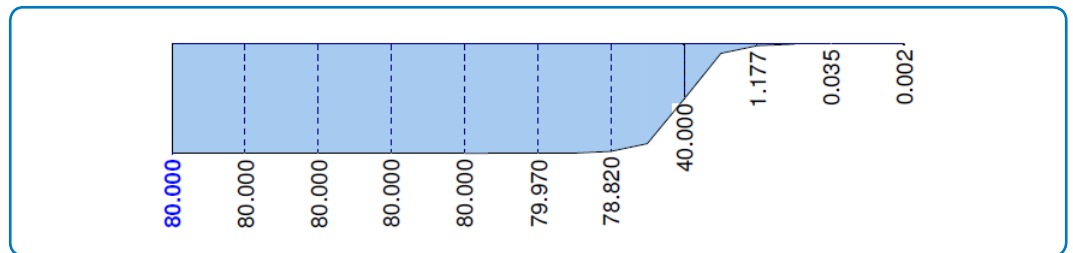


Figure 3: RFEM 5 – Primary torsional moment $M_{T\text{pri}}$ [kNm] behaviour

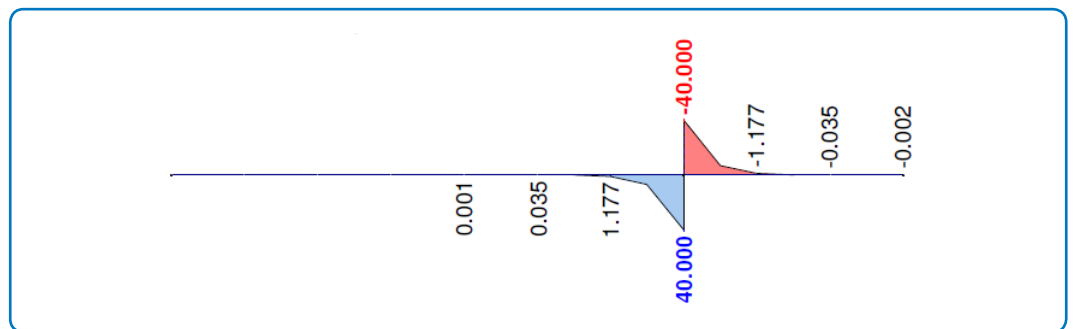


Figure 4: RFEM 5 – Secondary torsional moment $M_{T\text{sec}}$ [kNm] behaviour

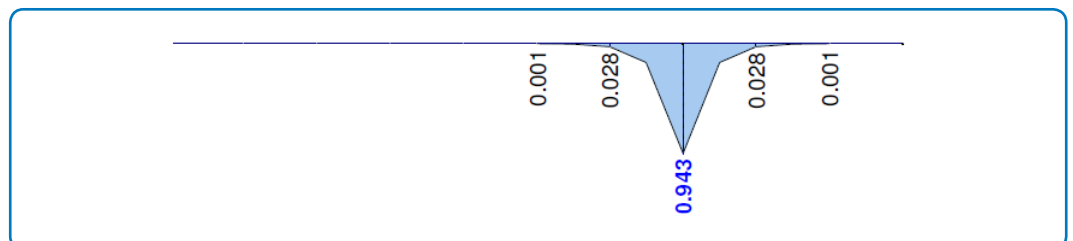


Figure 5: RFEM 5 – Warping moment M_ω [kNm²] behaviour

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The same task is also solved in RFEM 6 and RSTAB 9 with Torsional Warping Add-on. The results are shown in following graphs. It can be seen in RFEM 6 and RSTAB 9 results, there is no computational error due to the discretization.

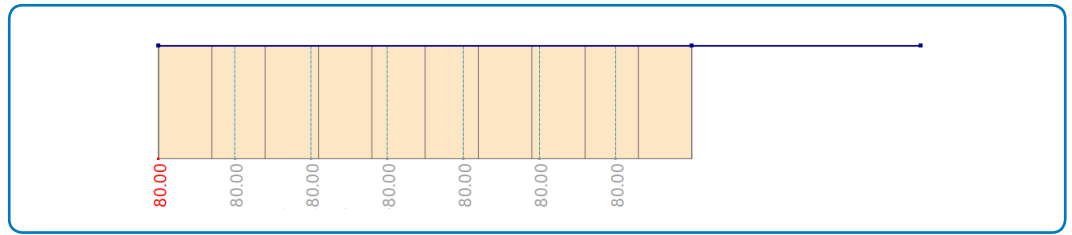


Figure 6: RFEM 6 – Total torsional moment M_T [kNm] behaviour

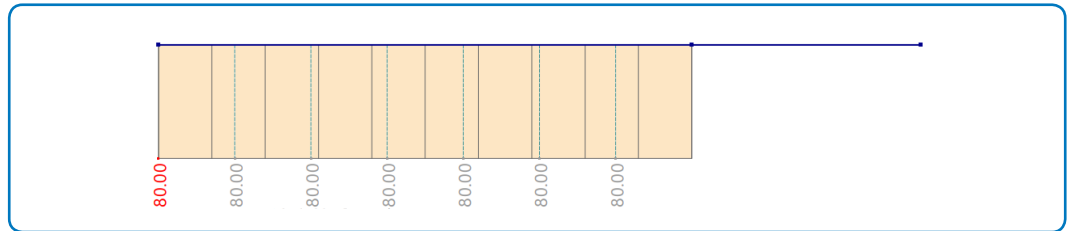


Figure 7: RFEM 6 – Primary torsional moment $M_{T_{pri}}$ [kNm] behaviour

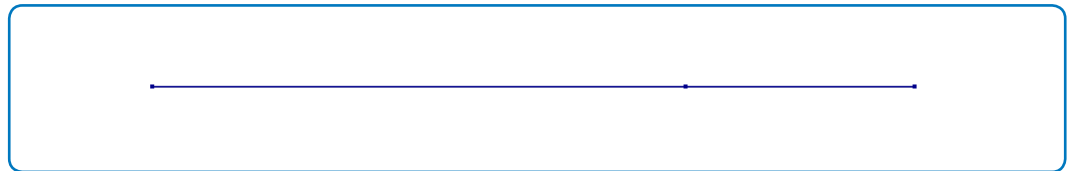


Figure 8: RFEM 6 – Secondary torsional moment $M_{T_{sec}}$ [kNm] behaviour

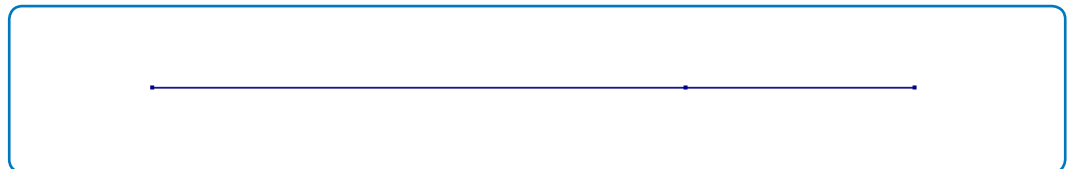


Figure 9: RFEM 6 – Warping moment M_{ω} [kNm²] behaviour

References

- [1] LUMPE, G. and GENSICHEN, V. *Evaluierung der linearen und nichtlinearen Stabstatik in Theorie und Software: Prüfbeispiele, Fehlerursachen, genaue Theorie*. Ernst, 2014.